



## Identification of a GTN damage model parameter set using HyperStudy

### Abstract

The damage model based on **G**urson, **T**vergaard and **N**eedleman (**GTN**) is nowadays often used in finite element analysis. There are different possible ways for the identification of the numerous parameters. In this approach, HyperStudy was used to achieve a first experience of the uniqueness and effects of the parameter sets.

**Matthias Schneider**

Salzgitter Mannesmann Forschung GmbH

Salzgitter, Germany

Phone +49-5341 21 4793

E-Mail: [M.Schneider@sz.szmf.de](mailto:M.Schneider@sz.szmf.de)

- Introduction: Feasibility of deep drawing steel parts
- Problem definition: Parameterisation of complex failure models
- Analysis: Parameter identification by virtual material testing
- Discussion: Uniqueness and usability of a GTN parameter set
- Conclusion: Parameter identification helps to understand the system



## Salzgitter AG Group

**External Sales cons.: €12.5 billion**

**Employees: 23915**

### Steel

Total Sales:  
**€3.0 billion**

Employees:  
**6,949**



### Tubes

Total Sales:  
**€2.2 billion**

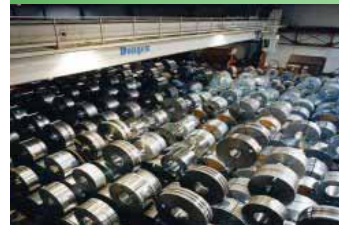
Employees:  
**5,929**



### Trading

Total Sales:  
**€5.6 billion**

Employees:  
**1,983**



### Technology

Total Sales:  
**€1.0 billion**

Employees:  
**4,907**

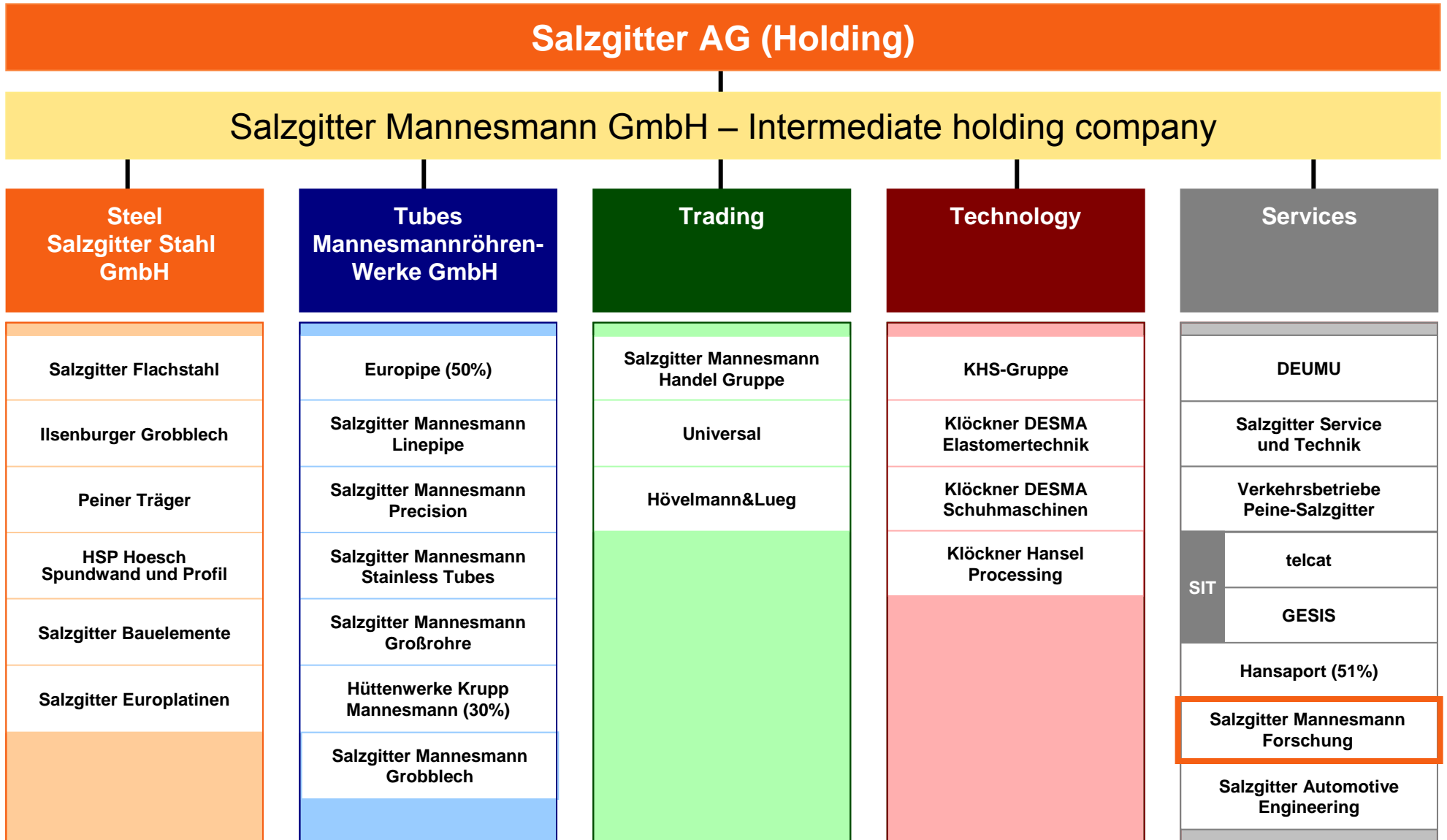


### Services

Total Sales:  
**€0.5 billion**

Employees:  
**4,003**





As of: December 31, 2008 | simplified structure

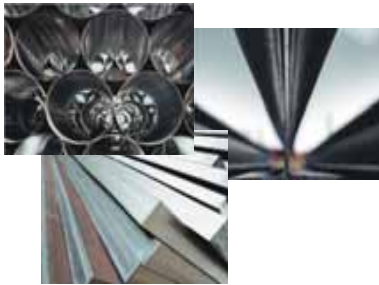
Figure 2

**products /  
customers**

**markets**

**research location:**

**Duisburg**



- ↻ tubes
- ↻ heavy plates
- ↻ profiles

- ↻ automotive  
(power train)
- ↻ machinery and  
plant construction
- ↻ energy sector
- ↻ construction (sections)

**research location:**

**Salzgitter**



- ↻ hot & cold rolled  
materials

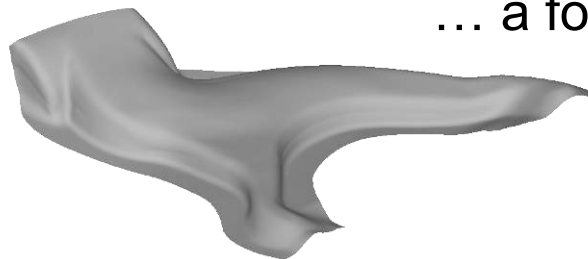
- ↻ automotive  
(body, chassis, ...)
- ↻ consumer industry
- ↻ construction  
(roof, wall, ...)

 SZMF supports the customer to ...

- ▶ ... chose the right steel grade for
- ▶ ... estimate the feasibility of
- ▶ ... reduce the weight of
- ▶ ... reduce the cost of
- ▶ ... optimise the forming processes of

 **Finite element forming simulation**

... a formed steel part!



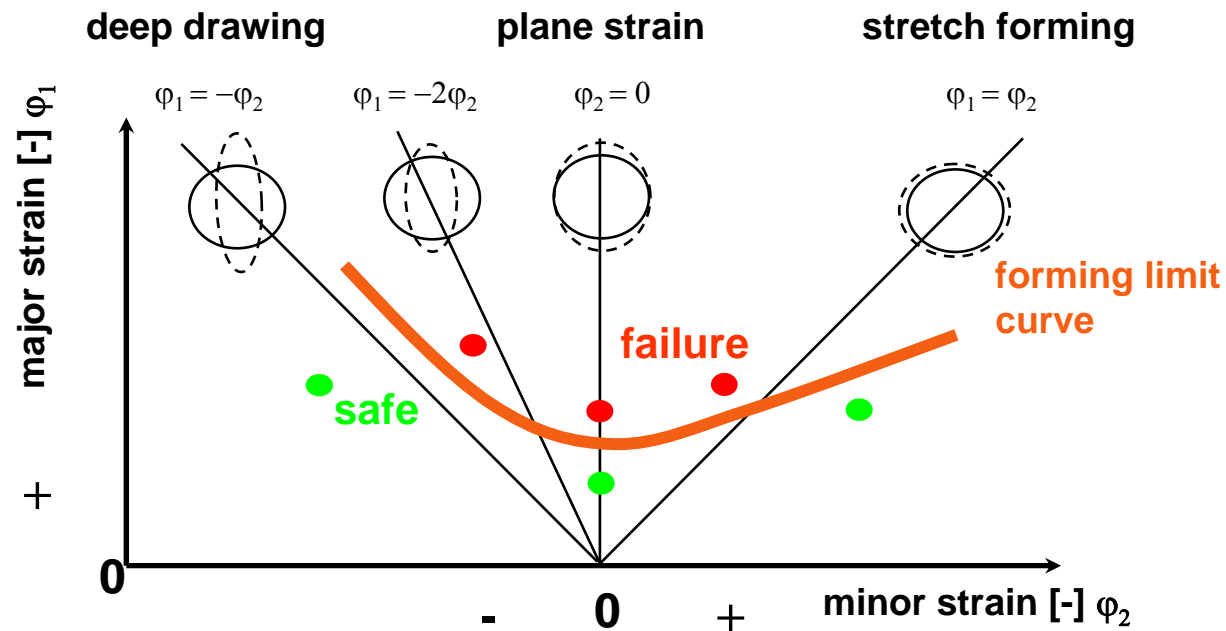
Sch07

 FE-Tools: **LS-Dyna, Pam-Stamp, HyperForm, (Ansys)**

 Failure criteria: **Forming limit curve (FLC)**

**FLC?**

➤ Determination of forming limit curves (FLC)



- ISO 12004
- ▶ Punch  $\varnothing$  100 mm
  - ▶ Thickness < 4.0 mm
  - ▶ Quasi-static
  - ▶ More than 5 geometries
  - ▶ 3 valid tests of each geometry

Alternatives to the FLC?

## Alternatives to the FLC:

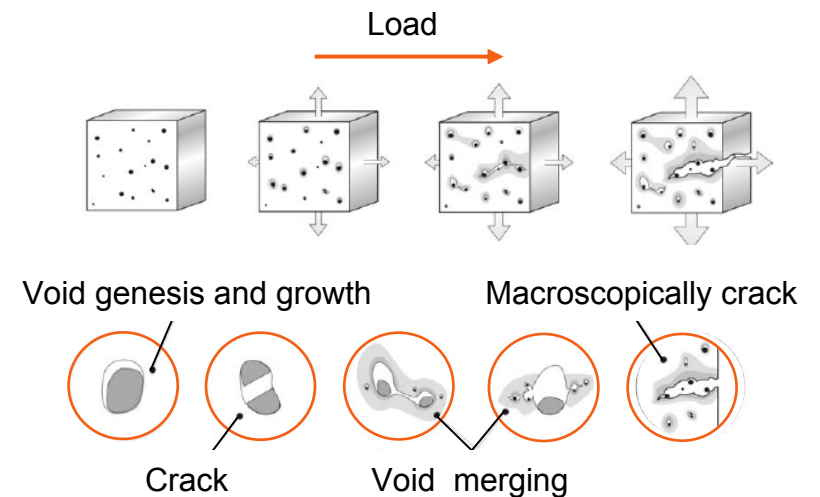
- ▶ Modifications of Nakajima
- ▶ Similar or additional tests
- ▶ Failure models

Model based on **Gurson, Tvergaard and Needleman**  
- Common and often used  
- Potentially good to access failure modeling

Gur77, Nee87

## Failure models:

- ▶ Advantages:
  - ▶ Strain path independence
  - ▶ “Memory” for pre-strains
- ▶ Disadvantages:
  - ▶ Complex models
  - ▶ Additional testing effort
  - ▶ Use of tests without standard



How to feed complex failure models?

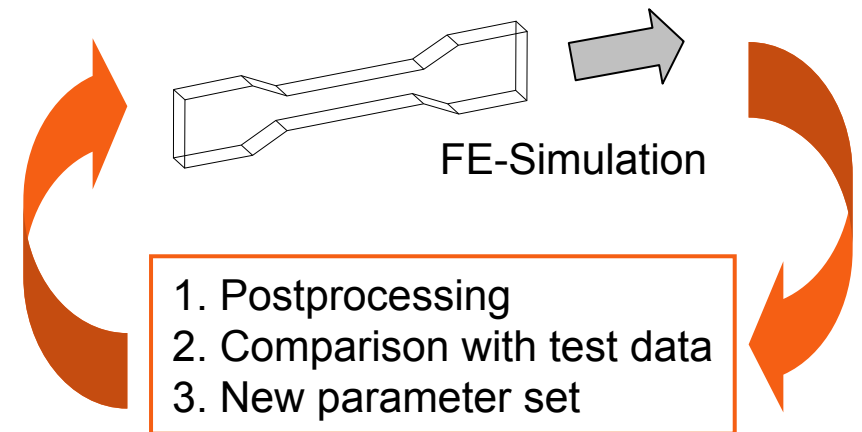
Figure 3 - Reu03

## Analysis approach

- Parameters of the GTN model:  $f_0, f_c, f_f, f_N, \epsilon_N, s_N$  Hal07
- Physical motivated: Additional tests, metallographic analysis
- Mathematical approximation: Use of parameter identification ←

### Parameter identification:

- FE-model of testing method
  - Target: parameter set with best match
- Method should be fixed by standard
- Results should be part of standard test
- Automated process
  - HyperStudy



Implementation?

## Analysis approach

FE-solver: LS-Dyna

Job management: Platform LSF®

Post processing:

Result read out: LS-Pre-Post controlled by scripts

Result comparison and abstraction: Fortran routines

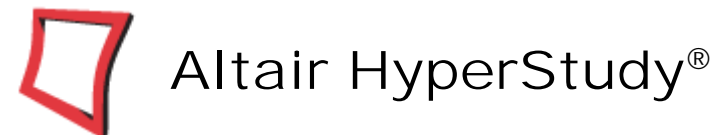
Parameter optimisation: HyperStudy

Design variables: 6

Vector sources: 10

Responses: 17

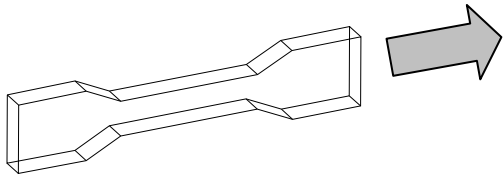
Constrains: 13



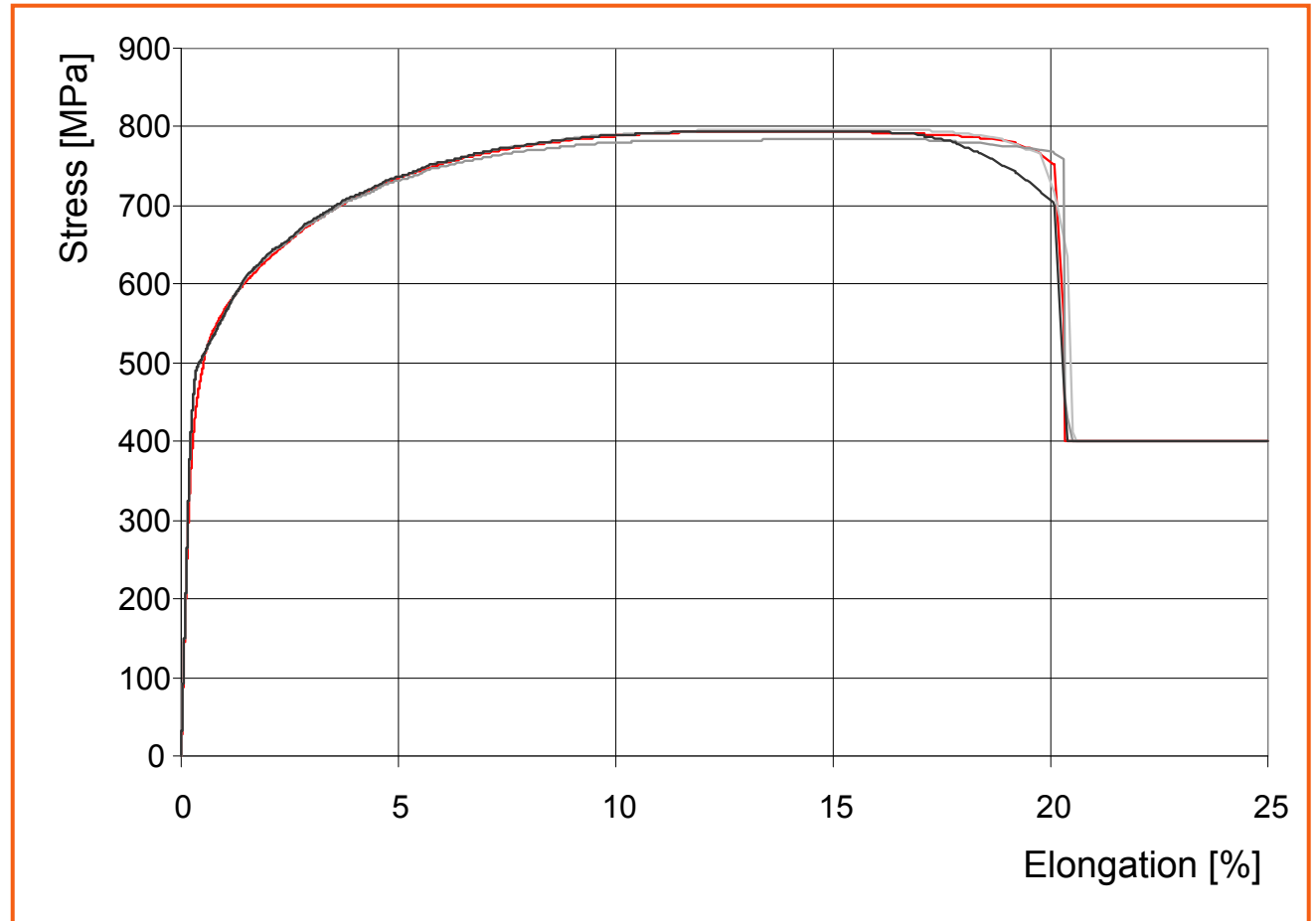
Optimisation algorithm: Genetic

Abort criteria: Minimal 15 generations (1900 runs) and 3 generations without improvement

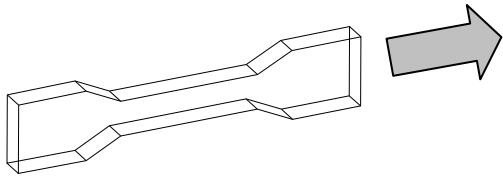
First step: tensile test



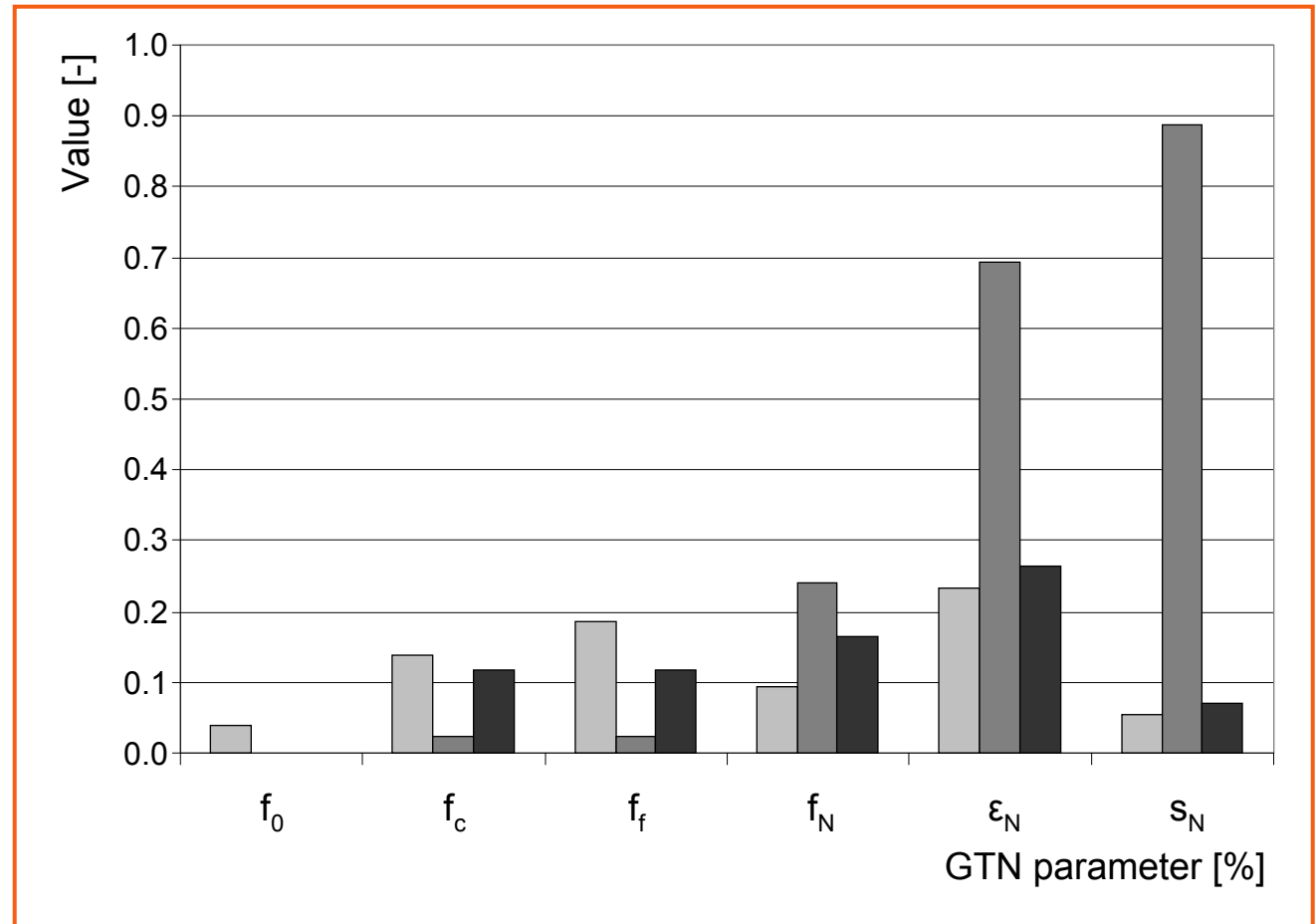
- ▶ **Real tensile test**
- ▶ GTN - 6 free parameters
- ▶ GTN - 2 parameters set by metallographic
- ▶ GTN - 2 step approach (before and after uniform elongation  $\epsilon_U$ )



Tensile test: Good matching

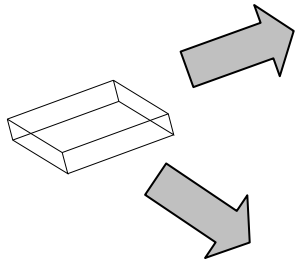


- ▶ GTN - 6 free parameters
- ▶ GTN - 2 parameters set by metallographic
- ▶ GTN - 2 step approach (before and after uniform elongation  $\epsilon_u$ )

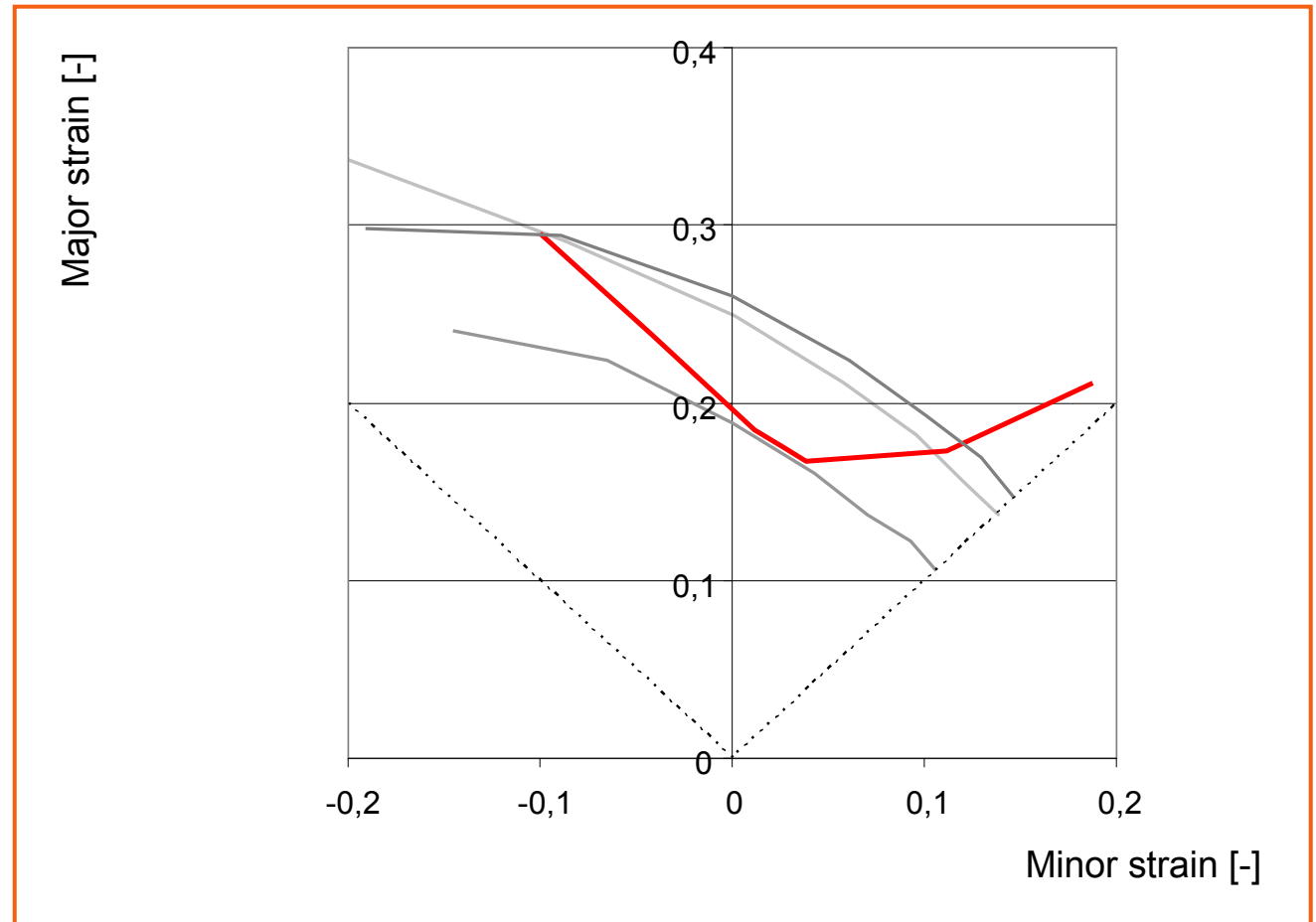


Tensile test:

Good matching  
No uniqueness

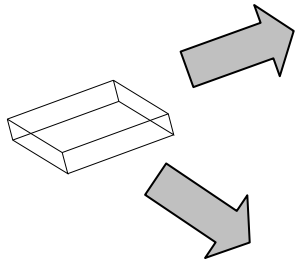


- ▶ **Real forming limit curve**
- ▶ GTN parameters optimised for **tensile test**
  - ▶ 6 free parameters
  - ▶ 2 parameters set by metallographic
  - ▶ 2 step approach (before and after uniform elongation  $\epsilon_u$ )

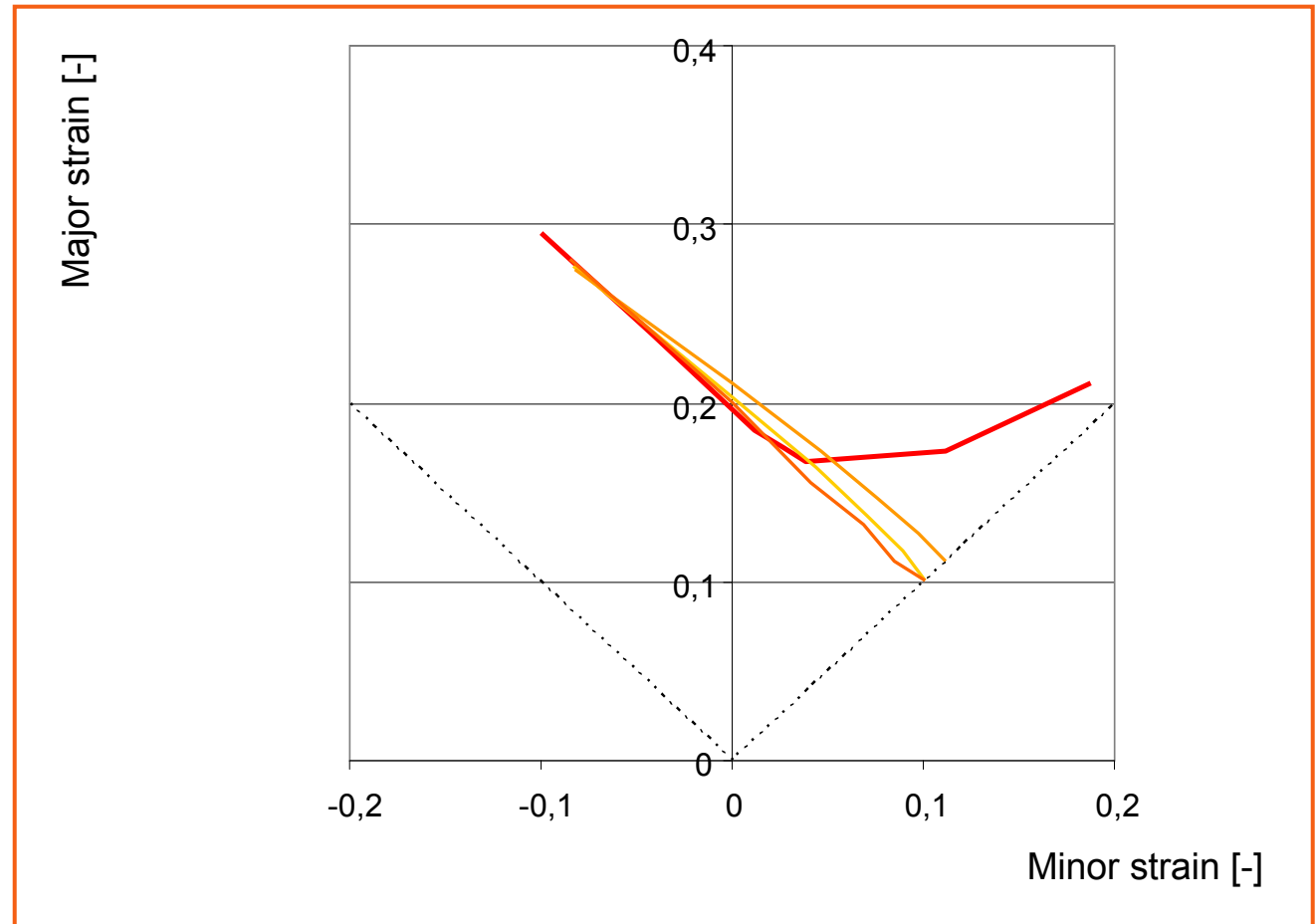


1-Element Nakajima:  
Next step:

Bad matching with parameter from tensile test  
Optimised FLC parameter set

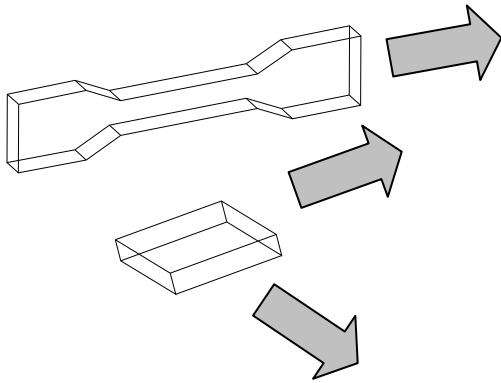


- ▶ **Real forming limit curve**
- ▶ GTN parameters optimised for **forming limit curve**
  - ▶ 6 free parameters
  - ▶ 4 free, 2 parameters set by metallographic
  - ▶ 6 free parameters focused on deep drawing and plane strain

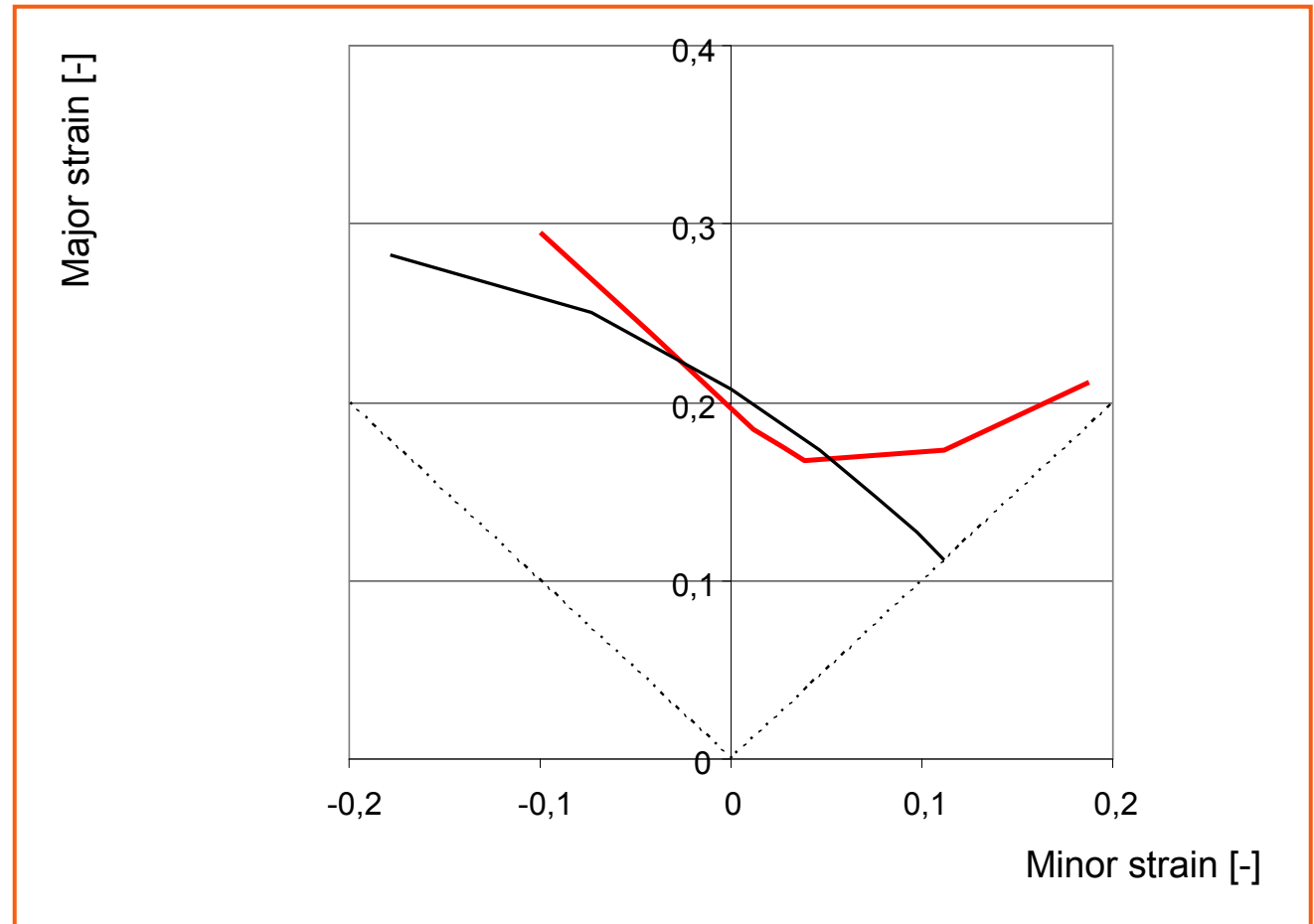


1-Element Nakajima:  
Next step:

Bad matching in stretch forming zone  
Combined optimisation



- ▶ Real forming limit curve
- ▶ GTN parameters optimised for **tensile test** and **forming limit curve**
- ▶ Tensile test deviation:
  - ▶ Uniform elongation = 1,6 %
  - ▶ Elongation = 0,2 %
  - ▶ Tensile stress = 19 MPa

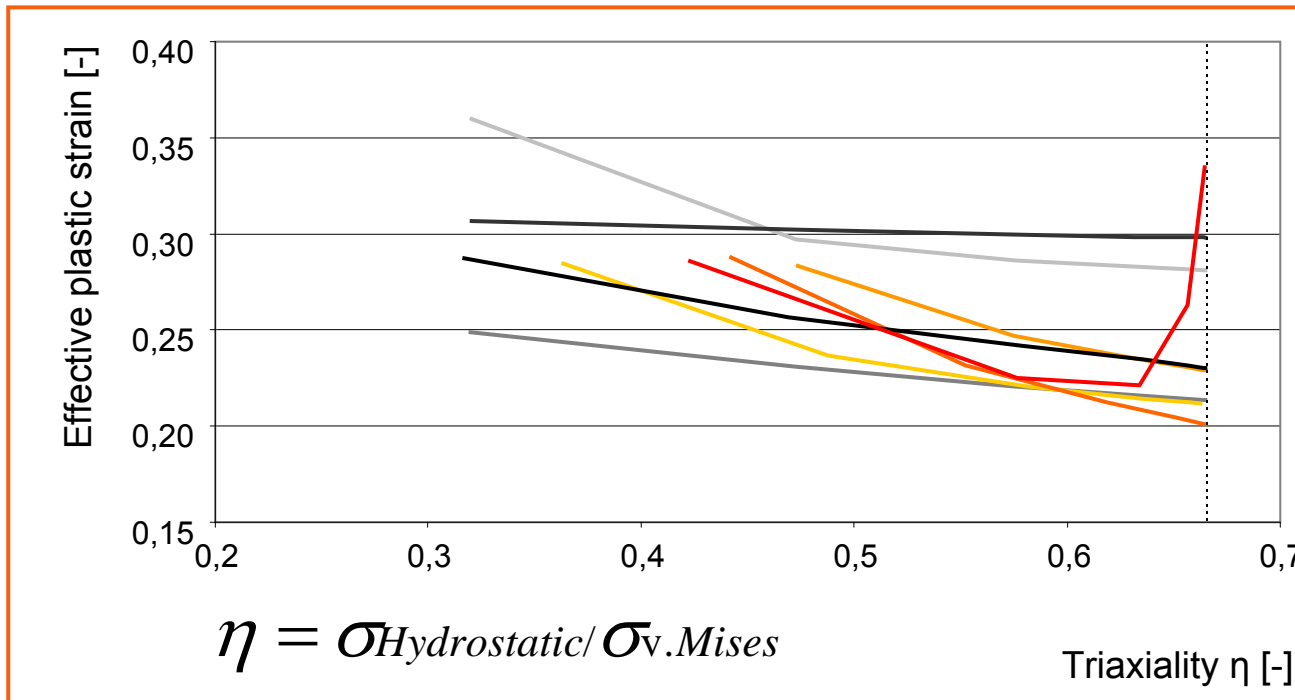


Combined test: Good matching of tensile test  
Acceptable matching on left half of FLC

➤ Matching tensile test: In the range of test scattering

➤ Matching forming limit curve:

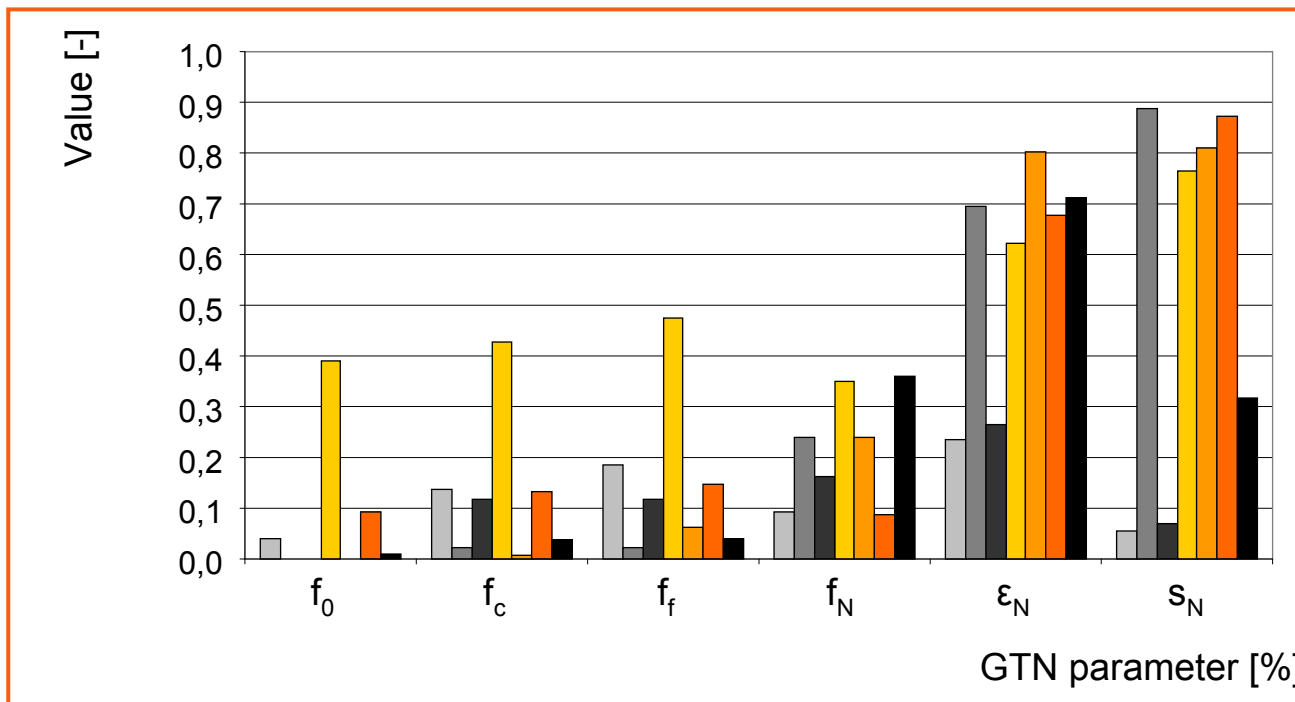
- GTN is not able to “rise” under stretch forming load
- Focus on “left side”



- Real FLC
- Tensile test 6 parameter
- Tensile test 4 parameter
- Tensile test uniform elongation
- FLC 6 parameter
- FLC 4 parameter
- FLC 6 parameter (dd and ps)
- Combined optimisation

Plot 6

- Matching tensile test: In the range of test scattering
- Matching forming limit curve: Focus on “left side”
- Uniqueness: Further investigations necessary
- Element size dependence: More complex optimisation necessary



Plot 7

## Conclusions

- Importance of failure models increases with launch of new more complex materials
- Adequate amount of tests for material and failure models makes them suited for daily use
- Parameter identification helps to reduce test amount and to get first impressions of the options of a system
- GTN failure model shows pros and cons
- There is a need for easy to use failure models with complex capabilities!



Everything is possible.

[www.salzgitter-ag.de](http://www.salzgitter-ag.de)



## Acknowledgements

The author thanks Mr. Sebastian Westhäuser for putting a lot of effort into his Diploma thesis. The results shown in this presentation are mostly based on his work in the Engineering and Simulation department of the Salzgitter Mannesmann Forschung GmbH in the year 2009.



## References

- Ebe08** Ebelsheiser, H.; Feucht, M.; Neukamm, F.: *“On calibrating advanced damage models using sheet metal coupon test”*, 7. LS-Dyna Anwenderforum, Bamberg, Germany, 2008
- Feu09** Feucht, M.; Haufe, A.; Neukamm, F.: *“Considering damage history in crashworthiness simulation”*, 7th European LS-Dyna conference, Salzburg, Austria, 2009
- Gur77** Gurson, A. L.: *“Continuum theory of ductile rupture by void nucleation and growth”*: Part I – Yield criteria and flow rules for porous ductile media, J. Eng. Materials and Technology 99, 2-15, 1977
- Hal07** Hallquist, J.O.: LS-Dyna User’s manual, Version 971 LSTC, 2007
- Nee87** Needleman, A.; Tvergaard, V.: *“An analysis of ductile rupture at a crack tip”*, J. Mech. Phys. Solids 35, 151-183, 1987
- Neu08** Neukamm, F.; Feucht, M.; Haufe, A.; Roll, K.: *“A generalized incremental stress state dependent model for forming and crashworthiness simulations”*, 805-810, 7th Numisheet, Interlaken, Switzerland, 2008
- Reu03** Reusch, F., *“Entwicklung und Anwendung eines nicht-lokalen Materialmodells zur Simulation duktiler Schädigung in metallischen Werkstoffen“*, Ph. D. thesis, Universität Dortmund, Germany, 2003
- Sch07** Schneider, M.: *“Verkürzung der Try-Out-Phase durch Prozessfenster-Ermittlung und Ziehsickenoptimierung”*, LS-DYNA Anwenderforum, Frankenthal, Germany, 2007

## Figures

1. Salzgitter AG - group structure
2. Salzgitter AG - companies
3. Schematic picture of GTN failure model
4. Identification routine

## Plots

1. Real and virtual tensile tests
2. GTN parameter optimised for tensile test
3. Forming limit diagram of parameter sets optimised for tensile test
4. Forming limit diagram of parameter sets optimised for FLD
5. Forming limit diagram of parameter set optimised for tensile test and FLD
6. Triaxiality diagram of all used parameter sets
7. GTN parameter of all used sets